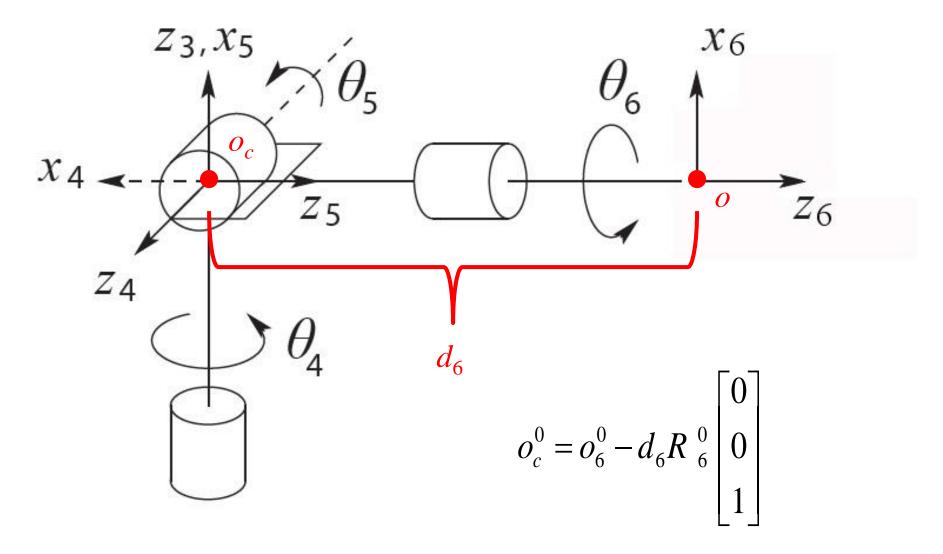
Day 9

Inverse Kinematics; Trajectory Generation



Inverse Kinematics Recap

I. Solve for the first 3 joint variables q_1, q_2, q_3 such that the wrist center o_c has coordinates

$$o_{c}^{0} = o_{6}^{0} - d_{6}R_{6}^{0}\begin{bmatrix}0\\0\\1\end{bmatrix}$$

- 2. Using the results from Step 1, compute R_3^0
- 3. Solve for the wrist joint variables q_4, q_5, q_6 corresponding to the rotation matrix

$$R_{6}^{3} = \left(R_{3}^{0}\right)^{T} R_{6}^{0}$$

for the spherical wrist

$$T_{6}^{3} = T_{4}^{3}T_{5}^{4}T_{6}^{5} = \begin{bmatrix} c_{4}c_{5}c_{6} - s_{4}s_{6} & -c_{4}c_{5}s_{6} - s_{4}c_{6} & c_{4}s_{5} & c_{4}s_{5}d_{6} \\ s_{4}c_{5}c_{6} + c_{4}s_{6} & -s_{4}c_{5}s_{6} + c_{4}c_{6} & s_{4}s_{5} & s_{4}s_{5}d_{6} \\ -s_{5}c_{6} & s_{5}s_{6} & c_{5} & c_{5}d_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

if
$$s_5 \neq 0$$

 $\theta_5^{\text{pos}} = \text{atan2}\left(\sqrt{1 - r_{33}^2}, r_{33}\right)$
 $\theta_5^{\text{neg}} = \text{atan2}\left(-\sqrt{1 - r_{33}^2}, r_{33}\right)$

$$T_{6}^{3} = T_{4}^{3}T_{5}^{4}T_{6}^{5} = \begin{bmatrix} c_{4}c_{5}c_{6} - s_{4}s_{6} & -c_{4}c_{5}s_{6} - s_{4}c_{6} & c_{4}s_{5} & c_{4}s_{5}d_{6} \\ s_{4}c_{5}c_{6} + c_{4}s_{6} & -s_{4}c_{5}s_{6} + c_{4}c_{6} & s_{4}s_{5} & s_{4}s_{5}d_{6} \\ -s_{5}c_{6} & s_{5}s_{6} & c_{5} & c_{5}d_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

for
$$\theta_5^{\text{pos}}$$
, $s_5 > 0$
 $\theta_4 = \text{atan2}(r_{23}, r_{13})$
 $\theta_6 = \text{atan2}(r_{32}, -r_{31})$

5

$$T_{6}^{3} = T_{4}^{3}T_{5}^{4}T_{6}^{5} = \begin{bmatrix} c_{4}c_{5}c_{6} - s_{4}s_{6} & -c_{4}c_{5}s_{6} - s_{4}c_{6} & c_{4}s_{5} & c_{4}s_{5}d_{6} \\ s_{4}c_{5}c_{6} + c_{4}s_{6} & -s_{4}c_{5}s_{6} + c_{4}c_{6} & s_{4}s_{5} & s_{4}s_{5}d_{6} \\ -s_{5}c_{6} & s_{5}s_{6} & c_{5} & c_{5}d_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

for
$$\theta_5^{\text{neg}}$$
, $s_5 < 0$
 $\theta_4 = \text{atan2} (-r_{23}, -r_{13})$
 $\theta_6 = \text{atan2} (-r_{32}, r_{31})$

6

• if $\theta_5 = 0$

$$T_{6}^{3} = T_{4}^{3}T_{5}^{4}T_{6}^{5} = \begin{bmatrix} c_{4}c_{5}c_{6} - s_{4}s_{6} & -c_{4}c_{5}s_{6} - s_{4}c_{6} & c_{4}s_{5} & c_{4}s_{5}d_{6} \\ s_{4}c_{5}c_{6} + c_{4}s_{6} & -s_{4}c_{5}s_{6} + c_{4}c_{6} & s_{4}s_{5} & s_{4}s_{5}d_{6} \\ -s_{5}c_{6} & s_{5}s_{6} & c_{5} & c_{5}d_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$=\begin{bmatrix} c_4c_6 - s_4s_6 & -c_4s_6 - s_4c_6 & 0 & 0\\ s_4c_6 + c_4s_6 & -s_4s_6 + c_4c_6 & 0 & 0\\ 0 & 0 & 1 & d_6\\ 0 & 0 & 0 & 1 \end{bmatrix}$$

continued from previous slide

$$= \begin{bmatrix} c_4 c_6 - s_4 s_6 & -c_4 s_6 - s_4 c_6 & 0 & 0 \\ s_4 c_6 + c_4 s_6 & -s_4 s_6 + c_4 c_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} c_{4+6} & -s_{4+6} & 0 & 0 \\ s_{4+6} & c_{4+6} & 0 & 0 \\ s_{4+6} & c_{4+6} & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
only the sum $\theta_4 + \theta_6$ can be determined

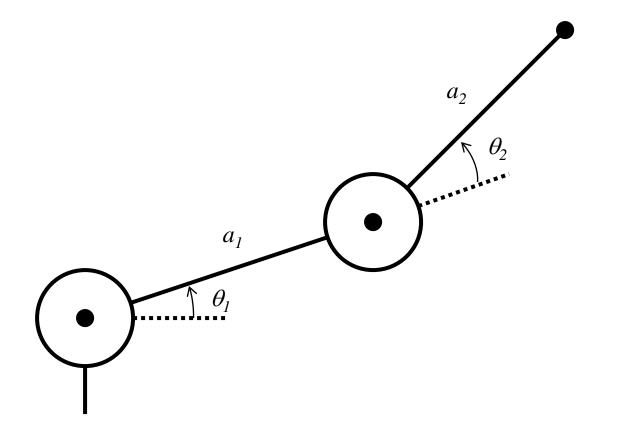
Using Inverse Kinematics in Path Generation

Path Generation

- a path is defined as a sequence of configurations a robot makes to go from one place to another
- a trajectory is a path where the velocity and acceleration along the path also matter

Path Generation

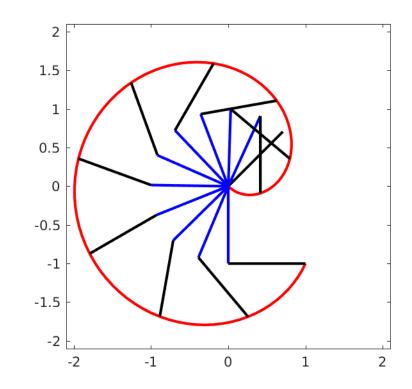
consider the 2-link RR robot

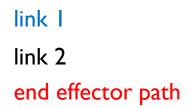


Path Generation

- suppose that the
 - initial configuration $\theta_1 = 45$ and $\theta_2 = -180$
 - final configuration $\theta_1 = 270$ and $\theta_2 = 90$

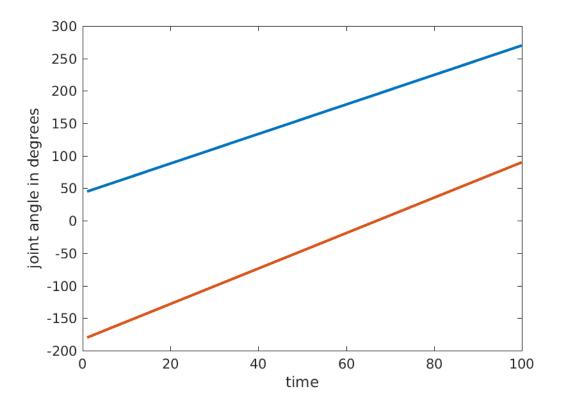
• a joint-space path is computed considering the joint variables





Joint-Space Path Joint Angles

Inear joint-space path



given the current end-effector pose

 ^{0}T

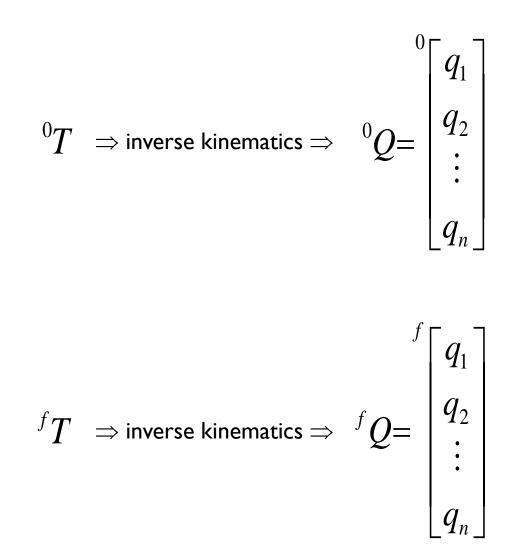
and the desired final end-effector pose

f T

find a sequence of joint angles that generates the path between the two poses

idea

- solve for the inverse kinematics for the current and final pose to get the joint angles for the current and final pose
- interpolate the joint angles

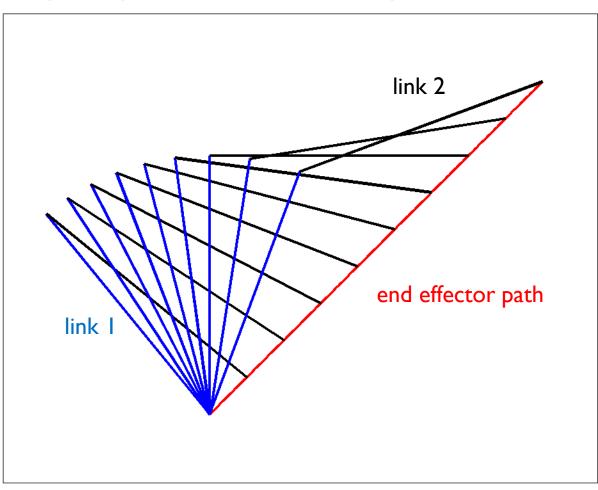


find ${}^{0}Q$ from ${}^{0}T$ (inverse kinematics) find ${}^{f}Q$ from ${}^{f}T$ (inverse kinematics) $\Delta t = 1 / m$ where m is the number of steps in the path $\Delta Q = {}^{f}Q - {}^{0}Q$ for j = 1 to m $t_i = j \Delta t$ ${}^{j}Q = {}^{0}Q + t_{j} \Delta Q$ set joints to ${}^{j}Q$ end

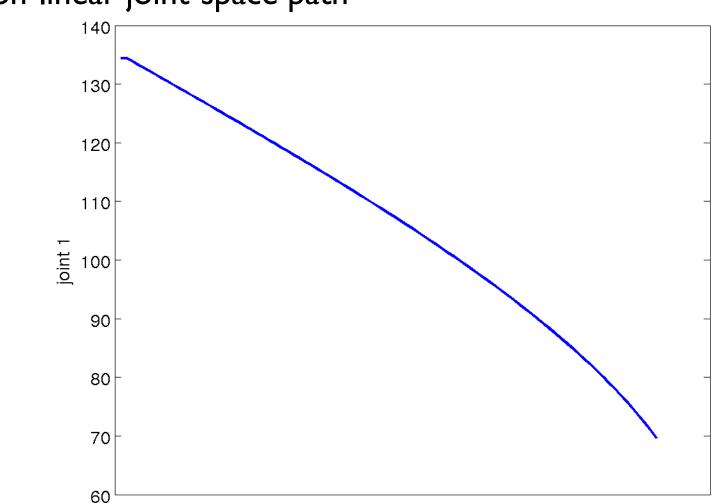
- Inearly interpolating the joint variables produces
 - a linear joint-space path
 - a non-linear Cartesian path
- depending on the kinematic structure the Cartesian path can be very complicated
 - some applications might benefit from a simple, or well defined, Cartesian path
 - e.g., move in a straight line, trace the shape of an object, move around objects in the workspace

Cartesian-Space Path

a Cartesian-space path considers the position of end-effector

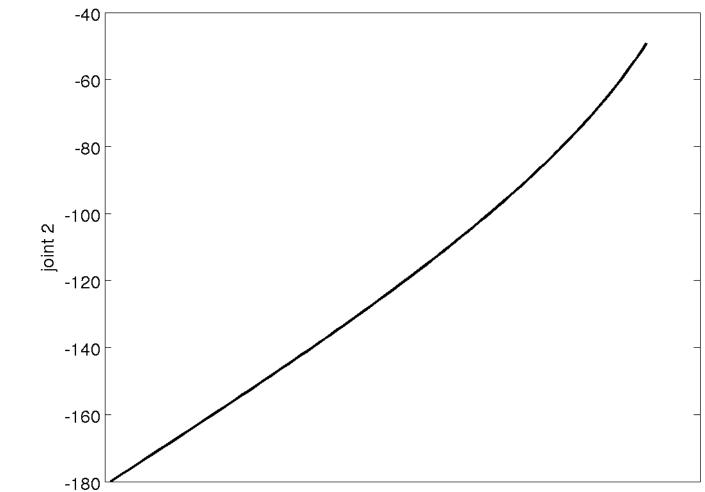


Cartesian-Space Path Joint Variable 1



non-linear joint-space path

Cartesian-Space Path Joint Variable 2



non-linear joint-space path

Cartesian-Space Straight Line Path

given the current end-effector pose

and the desired final end-effector position

find a sequence of joint angles that generates the straight line path between the two points

 $^{f}\mathcal{D}$

idea

- interpolate the between the current and final positions
- solve for the inverse kinematics at the interpolated positions to get the joint angles for the interpolated positions

Cartesian-Space Straight Line Path

 $\Delta t = 1 / m$ where m is the number of steps in the path $\Delta p = {}^{f}p - {}^{0}p$ for j = 1 to m $t_i = j \Delta t$ $^{j}p = ^{0}p + t_{j} \Delta p$ find ${}^{j}Q$ from ${}^{f}p$ (inverse kinematics) set joints to ${}^{j}Q$ end

Cartesian-Space Path

the previous straight line path algorithm only considered the position of the end effector

why?

what problem do you need to solve if you need to consider the pose of the end effector?